# NASA Technical Memorandum

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ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-9) LAUNCH

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Systems Dynamics Laboratory

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#### TECHNICAL MEMORANDUM

### ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-9) LAUNCH

#### I. INTRODUCTION

This report presents an evaluation of the atmospheric environmental data taken during the launch of the Space Shuttle/STS-9 vehicle. This Space Shuttle vehicle was launched from Pad 39A at Kennedy Space Center (KSC), Florida, on a bearing of 35 deg east of north at 1600 UT (1100 EDT) on November 28, 1983.

This report presents a summary of the atmospheric environment at launch time (L+0) of the STS-9, together with the sequence of prelaunch Jimsphere measured winds aloft profiles from L-14 hr through liftoff. The general weather situation for the launch and flight area is described, and surface and upper level wind/thermodynamic observations near launch time are given. Since the ship Redstone was unavailable for STS-9 duty, the SRB descent/impact atmospheric data were not taken. However, one can use the STS-9 ascent data for SRB studies, as the best substitute.

Previous MSFC-related launch vehicle atmospheric environmental conditions have been published as Appendix A of individual MSFC Saturn Flight Evaluation Working Group reports [1]. Office memorandums have been issued for previous flights giving launch pad wind information. A report has also been published [2] which summarizes most launch atmospheric conditions observed for the past 155 MSFC/ABMA-related vehicle launches through SA-208 (Skylab 4). Reports summarizing ASTP, STS-1, STS-2, STS-3, STS-4, STS-5, STS-6, STS-7, and STS-8 launch conditions are presented in References 3, 4, 5, 6, 7, 8, 9, 10, and 11, respectively.

#### II. SOURCES OF DATA

Atmospheric observational data used in this report were taken from synoptic maps made by the National Weather Service, plus all available surface observations and measurements from around the launch area. Upper air observations were taken from balloon-released instruments sent aloft from Cape Canaveral Air Force Station (CCAFS). High-altitude winds and thermodynamic data were measured by the Super-Loki rocketsondes launched from the CCAFS. Table 1 presents a listing of systems used to obtain the upper level wind profiles used in compiling the final ascent meteorological data tape. Data cutoff altitudes are also given in Table 1.

### III. GENERAL SYNOPTIC SITUATION AT LAUNCH TIME

A cold front, extending out of a low pressure area in Iowa, was passing through eastern Georgia and western Florida just prior to STS-9 liftoff. The influence of high pressure over eastern Florida was weakening as this front approached. Moderate, southerly winds bringing in warm temperatures and humid conditions prevailed throughout the early morning countdown period. Figure 1 presents the surface map conditions 4 hr before STS-9 launch. Figure 2 presents

the winds aloft conditions at the 500 mb pressure level 4 hr before launch. South-westerly to westerly winds dominated the flow aloft over the KSC Florida area.

Cloudiness increased throughout the morning of November 28, 1983, with the source being the frontal system located to the north and west of KSC. Figure 3 presents the GOES-5 visible picture taken at liftoff (1600 UT). Overcast skys consisting of 1/10 cumulus at 2500 ft, 3/10 stratocumulus at 5,500 ft and 10/10 cirrostratus at 30,000 ft were present during launch. Figure 4 shows an up-close visible shot of the Florida peninsula as recorded by GOES-5, taken at 1600 UT.

#### IV. SURFACE OBSERVATIONS AT LAUNCH TIME

Surface observations at launch time for selected KSC locations are given in Table 2. Included are pad 39A, shuttle runway, and CCAFS balloon release station observations. Neither precipitation nor lightning was observed at launch time.

Table 3 presents Pad 39A wind data along with other standard hourly meteorological measurements and sky observations for the 6-hr period prior to launch of STS-9. Values for wind speed and direction are given for the 84 m (275 ft) FSS reference level and 18 m (60 ft) pad light pole level.

#### V. UPPER AIR MEASUREMENTS DURING LAUNCH

The FPS-16 Jimsphere (1615 UT), MSS Rawinsonde (1604 UT), Super-Loki Rocketsonde (1800 UT), and Super-Loki Robin (1900 UT) systems were used to measure the upper level wind and thermodynamic parameters for STS-9 launch. At altitudes above the rocket-measured data, the Global Reference Atmosphere (GRA) [12] parameters for November KSC conditions were used. A tabulation of the STS-9 final meteorological data for ascent is presented in Table 4 which lists the wind and thermodynamic parameters versus altitude. A brief summary of parameters is given in the following paragraphs.

### A. Wind Speed

At launch time, wind speeds were 19.1 ft/sec (11.3 kn) at 60 ft and increased to a maximum of 117 ft/sec (69 kn) blowing from 252 deg. This maximum occurred at an altitude of 47,100 ft (14,356 m). The winds increased above this level as shown in Figure 5. The overall maximum measured speed was 249 ft/sec (147 kn) at 164,000 ft (49,987 m) altitude.

### B. Wind Direction

At launch time, the 60-ft wind direction was from the south (183 deg) and shifted through the southwest to become a westerly component above 33,000 ft (10,058 m). Winds remained in the winter-westerly regime at all measureable altitudes above this level. Figure 5 shows the complete wind direction versus altitude profile. As shown in Figure 5, wind direction became quite variable at altitudes with low wind speeds.

### C. Prelaunch/Launch Wind Profiles

Prelaunch/launch wind profiles presented in Figures 6 through 9 were measured by the Jimsphere FPS-16 system. Data are shown for the L-11 hr, L-7.25 hr, L-3.5, and L+0 measurement periods.

The wind speed and direction profiles for the 11-hr period prior to and including L+0 are shown in Figures 6 and 7. The in-plane (right crosswind) and out-of-plane (left crosswind) profiles are given on Figures 8 and 9. The wind speeds and component speeds were not significantly different from the November mean values in the 30,000 to 50,000 ft layer during the period for which data are shown.

### D. Thermodynamic Data

The thermodynamic data taken at STS-9 launch time, consisting of atmospheric temperature, dew-point temperature, pressure, and density have been compiled as the STS-9 ascent meteorological data and are presented in Table 4. The vertical structure of temperature for the STS-9 ascent is shown graphically versus altitude in Figure 10.

The atmospheric thermodynamic parameters of temperature, pressure, and density, measured during STS-9 launch below 113,000 ft (34,442 m) were all within 6 percent of their respective PRA-63 [13] annual values. All these parameters stayed within 19 percent of their respective PRA-63 values, at all levels of measurement.

### E. SRB Upper Air and Surface Measurements

As has been mentioned in the introduction, since there was no ship available, an SRB descent meteorological data tape has not been constructed. The tabular values for the ascent meteorological tape as presented in Table 4 should be used for SRB descent/impact studies since it is the closest measured data source.

### VI. ATMOSPHERIC SUMMARY CONDITIONS FOR STS LAUNCHES

Given in Table 5 are selected atmospheric L+0 launch conditions for all the Space Shuttle launches.

TABLE 1. SYSTEMS USED TO MEASURE UPPER AIR WIND DATA FOR STS-9 ASCENT

	Date: No	November 28, 1983		Portion of	Portion of Data Used	
3	Release Time	Time	Start		End	77
Type of Data	Time (UT) (hr:min)	Time After L+0 (min)	Altitude m (ft)	Time After L+0 (min)	Altitude m (ft)	Time After L+0 (min)
FPS-16 Jimsphere	16:15	15	6 (21)	15	17,373 (57,000)	74
MSS Rawinsonde	16:04	4	17,678 (58,000)	62	29,870 (98,000)	102
Super-Loki Rocketsonde (Datasonde)	18:00	120	65,227 (214,000)	120	30,175 (99,000)	138
Super-Loki Rocketsonde (Robin)	19:00	180	82,601 (271,000)	180	65,532 (215,000)	181

TABLE 2. SURFACE OBSERVATIONS AT STS-9 LAUNCH TIME

							Sky	Sky Cover		Wind	p
Location <sup>a</sup>	Time After L+0 (min)	Pressure (MSL) N/cm <sup>2</sup> (psia)	Temperature °K (°F)	Dew Point °K (°F)	Relative Humidity (%)	Visibility km (miles)	Cloud** Amount	Cloud Type	Height of Base Meters (ft)	Speed ft/sec (kt)	Direction (deg)
NASA Space Shuttle Runway X68e	i G	10.159 (14.734)	298.6 (77.8)	293.2 (68.0)	7.2	16 (10)	н	Strato- Cumulus	762 (2,500)	16.9 (10.0)	180
Winds Measured at 10.4 m (34 ft)							က	Strato- Cumulus	1,676 (5,500)		
				-14	oming <u>, yearn</u> gand		10	Cirro- Stratus	6,401 (21,000)		
CCAFS <sup>C</sup> Surface Measurements	Ħ J	10.156 (14.730)	298.3 (77.2)	294.3 (70.0)	4.6	16 (10)	<del></del>	Cumulus	762 (2,500)	18.6 (11.0)	160
					,		10	Cirrus	6,401 (21,000)		
Pad 39A Lightpole SE 18.3 m (60.0 ft)	.0	10.159* (14.734)	297.6 (76.0)	294.5 (70.3)	83	į	ı	1.	t	19.1 <sup>b</sup> (11.3)	183 <sup>b</sup>
Pad 39A FSS (Top SE) 83.8 m (275 ft)	0	1	1	l	ı	ı	1	t	:	32.0 <sup>b</sup> (18.9)	190 <sup>b</sup>

\*Pad 39A Camera Site 3 barometric pressure instrument appeared to be reading too high. Therefore, the KSC Shuttle runway station pressure value interpolated to  $10.153 \text{ N/cm}^2$  at 21 ft above MSL was used as the L+0 pad atmospheric pressure measurement.

\*\*Ten-tenths total sky cover.

a. Altitudes of measurements are above natural grade, except where noted.

b. Approximately 1 min average prior to L+0.

c. Balloon release site.

d. Pad 39A thermodynamic measurements are taken at camera site No. 3, approximately 6.4 m (21 ft) above MSL.

e. Official STS-9 sky observational site.

STS-9 PRE-LAUNCH THROUGH LAUNCH KSC PAD 39A METEOROLOGICAL MEASUREMENTS<sup>a</sup> TABLE 3.

		Other Remarks			<del></del>	in the property of	· · · · · · · · · · · · · · · · · · ·	<u> </u>	
Q		V1S. (mi)	10	10	10	10	10	10	10
Sky Condition <sup>b</sup>	Total	Sky	3/10	2/10	4/10	9/10	9/10	10/10	10/10
Sky C		Clouds	Scattered at 3,000 ft Scattered at 21,000 ft	Scattered at 3,000 ft Scattered at 10,000 ft	Scattered at 2,500 ft Scattered at 9,000 ft Scattered at 30,000 ft	Scattered at 5,000 ft Broken at 30,000 ft	Scattered at 2,500 ft Scattered at 6,000 ft Broken at 30,000 ft	Scattered at 2,500 ft Scattered at 5,500 ft Overcast at 30,000 ft	1/10 SC at 2,500 ft 3/10 SC at 5,500 ft 10/10 CS at 30,000 ft
	o c	WD°	180	170	200	190	170	140	183
	60' Level (SE) <sup>C</sup>	WS Kt	12	12	œ	œ	4.	14	11
ß	evel c	WD°	210	210	250	260	230	240	190
surement	275' Level (SE) <sup>C</sup>	WS Kt	35	33	28	25	28	25	19
ic Mea	E C	(%)	100	100	66	66	68	82	83
nospher	Dew	(°F)	72	72	69	73	70	69	20
Hourly Atmospheric Measurements	r c	(°F)	72	72	20	7.3	73	74	76
Ĥ	98 Nowbow 1009	Time UT	1000	1100	1200	1300	1400	1500	L+0 <sup>d</sup> 1600

a. Hourly observations obtained verbally from CCAFS.

b. Sky observations taken at the Shuttle runway site X68.

c. 10 min mean about the hour from pad 39A instrumentation.

L+0 PAD Wind and thermodynamic parameters obtained from HOSC strip charts. SE Anemometers used at 60 and 275 ft levels for L+0 wind conditions (approximately 10 sec average prior to L+0). Pad 39A L+0 atmospheric pressure, at 21 ft (MSL), was 10.153 N/cm<sup>2</sup>. Sea level pressure was 10.159 N/cm<sup>2</sup>. ٥.

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TABLE 4. (Continued)

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DEW POINT	-28.2	2	-28 · d	-28.5	-28.6	9.82-		28.0	-29° n		-28.3	4.75-	9-92-	-25.8	-25.0	1.42-		-21.6	-20.8	-21.1	-21.5	-21.8	-22.1	2	-22.8	-23.1	123.4		-25.2	-26.3	-27.3	-28.4	-29.5	9.00	7.51.	) M	i i		-34.1	-33.7	E 900	-32.9	-32.5	-32.1	-31.7	-31.3
DENSITY (GRAM/M3)	.6438+03	.6418+33	•6399+03	.6379+93	.6360+03	66 3 4 D 4 D 3	201700	*0.00*	46263473	*6244+03	.6225+03	•6206+03	.6188+03	.6169+03	.6151+03	•6132+113 •••••••	10.440.4 40.440.4	.6377+03	6059+03	.6038+03	.6018+03	. 5097+33	.5977+03	.5957+03	.5936+33	.5916+73	* 0040400	100 - 00 - 00 - 00 - 00 - 00 - 00 - 00	3 0 0	13+7	192+1	770+0	1+07/	# 07/28 + 03	0.0	7. E. S.	E+##9	624+7	605+7	58.5	565+7	546+0	30	10	3	.5468+73
PRESSURE (MILLIBARS)	4875+0	956+0	836+0	817+D	198+D	. 47804 60.036	70.40	723+	705+0	686+0	0+149	9	0+029	612+0	594+	# 45/5+U3:	1023	3 6	503	488+	. 4467+03	+611		4 7 7 7	396+	*4378+D3	100	3.00	30.0	0	574+	256+0	<b>6</b>	0+727		*	4 10	178+0	121+	4 5 5	19.8+	971.4	7.5+	138+	772+	•
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w 6	19501	214	- 6 - 7 - 1	215	217	215	216	214	219.	220	2.9	224	217	229	221	223		224	227	231	230	235	A Commence of the Commence of	236	2.0	D M	20.4		240	244	242	243	245	245	94.6	245	24#	243	242	242	241	242	242	241	243	241	240	
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<b></b> +	0.35.00	2000	00000000000000000000000000000000000000	25300	02050	125500	125610	J.25 7 Jul	U25 900	225900°	uz6-900°	126100	226230	026300	326 a D C	C26500	026640	226700	G2680T	0.26.900	027000	027100	02720	027300	705757	027500	004.464	2278CD	327200	228000	028100	028200	028300	10.28.40.0 0.38.40.0	000000	028400 028400	028400	U2890D	03000	026100	029200	U29 300	029400	0295uñ	029600	02620	008.620 008.620	

TABLE 4. (Continued)

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(MILLIBARS)	230+0	216+0	202+	0 4 6 4 7	240	148+0	35	0	108+g	0+5+0	092	# 4 00 i	* (155+03 * 7742+03	ロングナロ	. 4	03+0	0+066	0+110	1000	2 6	926+0	913+0	0+106	20488403	142 40	851	838+D	826+0	913+0	10040	777+0	0+1197	52+0	0.00	716+0	704+	20	680+	÷ 29.5	4 4 4 4 4	, W	600
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-	30.1	30.5	30300		5. U.S.	) C	30.0	30.0	31.7	311	C) :	-	3 7 7	ີ •~ 	, <b>,</b> ,	31.9	310	323	5. C	032300	27	32.5	325	32.4	7 6	)	33.1	332	20 P	. U. . M . M	335	337	1 M	7 C		342	343	17	34.5	2 to 2	- 0)	1 2 2 2

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PRESSURE	[	0+019	• 25°8+03	587+0	575+0	2	MO+00000.	0	530+0	519+E	20	0+904	4 2 2 + O	*	44 W	5	<b>*</b> *	m,	2		2397+03	9 1	2375+03	٠ د د	2354+03	, t	3340	٠ ٠	301+0	290+0	.2280+03	.2270+03	ů.	2249+03	0 4	) C	9 60	0+86	197+0	177	167+0	57+0	147+0	2137+03	127+	20+74154 2450450	- 0	9 8 0
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NIND DIRECTION	25.0	259	0.00	260	260	259	258	258	259	259	258	257	257	- 0 Y	264	- C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C-C	255	256	200	255	254	255	255	254	0 N	25.4	100 C. Commence of Co.	252	252	253	254	ارا و د ا	256	257	257	257	257	257	60 60 60 60 60 60 60 60 60 60 60 60 60 6	258	7.52	257	1126	256	S)	255
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NIND DIRECTION	324	254	722	224	226	2.29	231	234	237	237	238	240	242	- E	254	256	25.9	261	258	256	2 2 3	238	230	224	220	219	205	192	181	199	226	280	295	(5) (5)	293	1991	2.67	7.00	080	278	268	260		Manager   100	254
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TABLE 4. (Continued)

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PRESSURE (MILLIBARS)	e-	.1914+02	.1826+02	.1743+02	704440	1517+02	.1448+02	.1393+02	.1320+02	.1260+02		_	1096+02	- 1046+UZ	9 5	9102+01	8691+01	. ±	10+6264	575	. 7237+01	915+	10+60999	317+	• 5039+01	5774+01	#0+000 h .	10.75.75. 10.48.05.	. 4837+01	• 4630+01	. 4433+01	4245+01	#D+990p*	10+0×0×0×	576+	+12h	. 7294+D1	146+	*	10+1080.	• 2780+01	658+	561+	+0.04 40.04 40.04	10+1400	10.2
TEMPERATURE (DEG C)	-54.8	4	-53.1	- C		7.00-	٠ ښو ن	50.	50.	The state of the s	2.1	ر در	52.	-52.0	• • • •	4 0	00	•	- 48 a	-47.8	-47.2	÷	-45.9	M • 10 37 -	• -	ņ,	D. 24-		-39.1	-39.2	-36. <b>6</b>	-34-8	M P	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	22.9	- 31 • 8	-39.2	-28.6	-27.0	Š	~	-22.5		· /	7	-
WIND DIRECTION	257	285	٠	٠Ô.	n F	27.0		<u></u>	257	256	256	ھ	264	712	ט ויי	692	261	257	265	274	280	œ.	285	άn	288	<u> 167</u>	300	289	60	217	-	٠	Ö	οv	265	•	263	261	262	9	292	261	9	6	267	. 0.7
WIND SPEED (FT/SEC)	C33		3	J :	# 4	0 a a c	- 37	4	#	LC.	S	S	ď.	9 4	0 4	7 C	<b>-</b> α	) (C)	0	-	C	6	o.	0	Ó. 1	oo r	٠,	V 35-0	9	-	~	0	നെ	oα	0	0	0	***	N	0	m	M	m	w, t	~ ~	^
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TEMPERATURE	(DEG C)	-77	-78.5	-79.1	-78.5	-77.3	-76.1	-75.0	73.8	-72.2	-70.2	-68.1	-66.1	-64.0	-62.0	-59.1	-56.2	-53.2	E 600 -	4.7.4	-43.7	-39.3	-34.8	-30.3	-25.9	-21.4	-14.5		6.1	5 • 9	12.8	23.6	29.5	38.7		58.0	68.0	78.2	2.84
WIND DIRECTION	(DEG)	205	480	450	289	275	C. C.	271	27.0	269	269	965	569	269	26P	268	267	265	256	116	190	389	101	104	108	101	105	109	211	121	120	118	124	130	136	143	150	157	164
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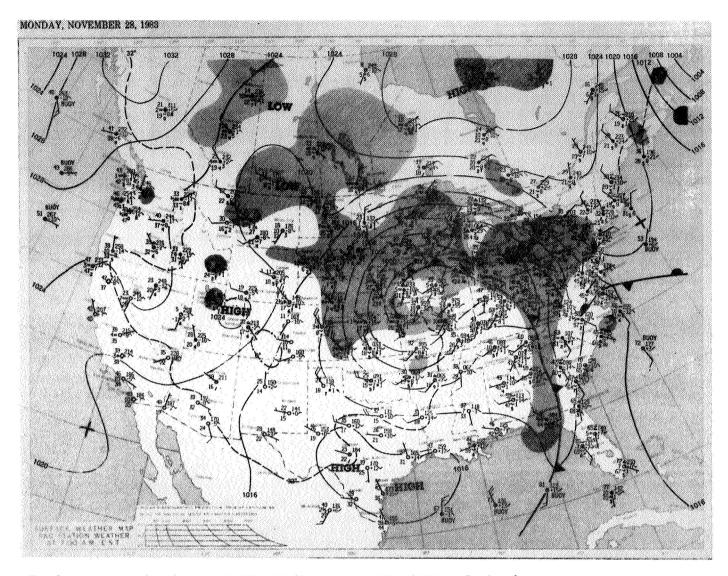
SELECTED ATMOSPHERIC OBSERVATIONS FOR THE FLIGHT TESTS OF THE SPACE SHUTTLE VEHICLES TABLE 5.

	Count Down and Launch Comments r. of Meteorological Significance			0.	9.	O Wind directional change observed at Pad just prior to L+0.8	6.	9		∞	9 17 min countdown delay due to adverse weather conditions.	7
	Inflight Conditions Max. Wind Below 60,000 ft		Dir. (deg)	250	286	250	329	336	277	278	349	252
			Speed (ft/sec)	86	158	119	37	146	155	9/	30	117
			Alt. (ft)	44,300	36,300	45,000	47,900	40,600	46,100	45,900	45,100	47,100
	Surface Observations	Wind <sup>b</sup>	Dir. (deg)	125 120	345 355	50 <sup>f</sup> 145 <sup>f</sup>	133i 141i	8 8	63 55	$\frac{10^{\mathrm{f}}}{350^{\mathrm{f}}}$	269 268	183
			Speed (ft/sec)	11.8	27.0 27.0	7.0 <sup>f</sup> 8.0 <sup>f</sup>	5.8 <sup>i</sup> 4.9 <sup>i</sup>	22.0 35.0	12.7 16.4	5.9 <sup>f</sup> 10.3 <sup>f</sup>	8.8 14.0	19.1
		Thermodynamic <sup>a</sup>	Rel. Hum. (%)	82	61	71	67	89	55	80	26	83
			Temp. (°C)	21	23	24	53	22	23	25	24	24
			Press <sup>d</sup> N/cm <sup>2</sup>	10.234 <sup>e</sup>	10.166	10,160	10.200	10.227	10,183	10.146	10.111	10.153
		Vehicle Data	Launch Pad	39A	39A	39A	39A	39A	39A	39A	39A	39A
			Time <sup>c</sup> (EST) Nearest Minute	0020	1010	1100	1100 <sup>h</sup>	0719	1330	0733 <sup>h</sup>	0232 <sup>h</sup>	1100
			Launch Date	4/12/81	11/12/81	3/22/82	6/27/82	11/11/82	4/4/83	6/18/83	8/30/83	11/28/83
			Vehicle No.	STS-1 Columbia	STS-2 Columbia	STS-3 Columbia	STS-4 Columbia	STS-5 Columbia	STS-6 Challenger	STS-7 Challenger	STS-8 Challenger	STS-9 Columbia
	<del> </del>		Seq. No.		7	м	4	'n	9	7	∞	6

a. Pad 39A thermodynamic measurements taken at approximately 1.2 m (4 ft) above natural grade at camera site No. 3.
b. 1 min average prior to L+0 of 60 ft PLP (listed first) and 275 ft FSS winds measured above natural grade.
c. Eastern Standard Time unless otherwise noted.
d. Pressure measurement applicable to 21 ft above MSL unless otherwise indicated.
e. Pressure measurement applicable to 14 ft above MSL.

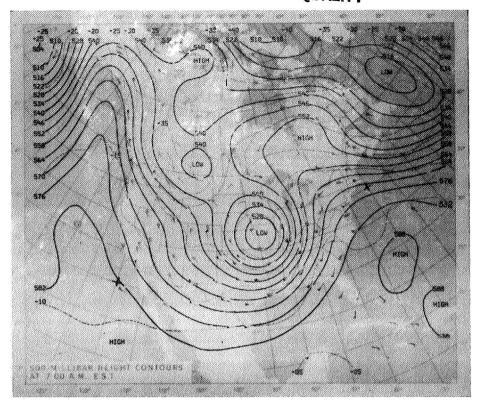
f. 10 sec average prior to L+0.g. Due to onset of sea breeze.h. Eastern Daylight Time.

i. 30 sec average prior to L+0.



Surface Synoptic Map at 1200 UT November 28, 1983 - Isobaric, Frontal, and Precipitation Patterns are Shown in Standard Symbolic Form.

Figure 1. Surface synoptic chart 4 hr prior to launch of STS-9.



500 Millibar Height
Contours at 1200 UT
November 28, 1983.
Continuous Lines Indicate Height Contours In Feet
Above Sea Level. Dashed Lines are Isotherms In
Degrees Centigrade. Arrows Show Wind Direction
and Speed at the 500 MB Level.

Figure 2. 500 mb map 4 hr prior to launch of STS-9.

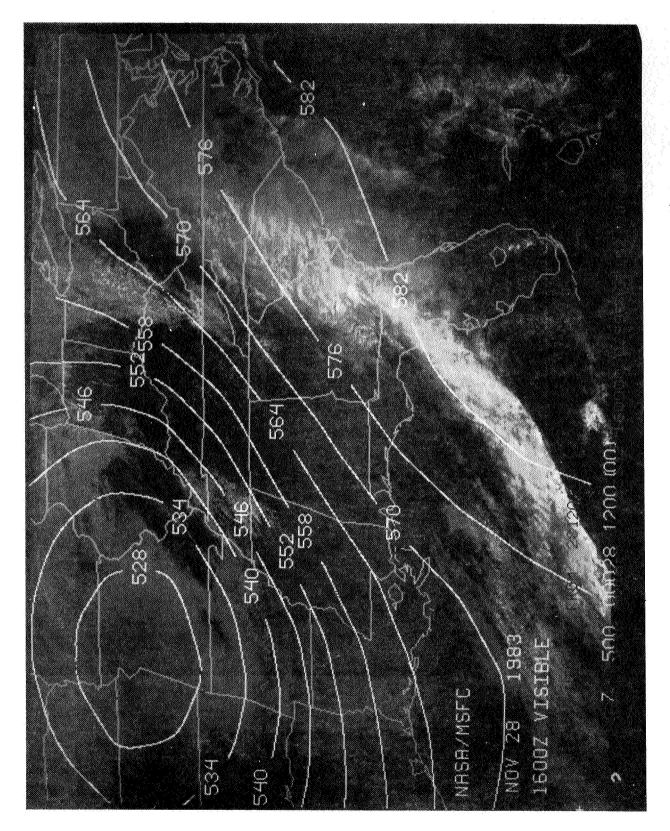


Figure 3. GOES-5 visible imagery of cloud cover at time of launch of STS-9 (1600 UT, November 28, 1983). 500-mb contours and wind barbs are also included for 1200 UT.

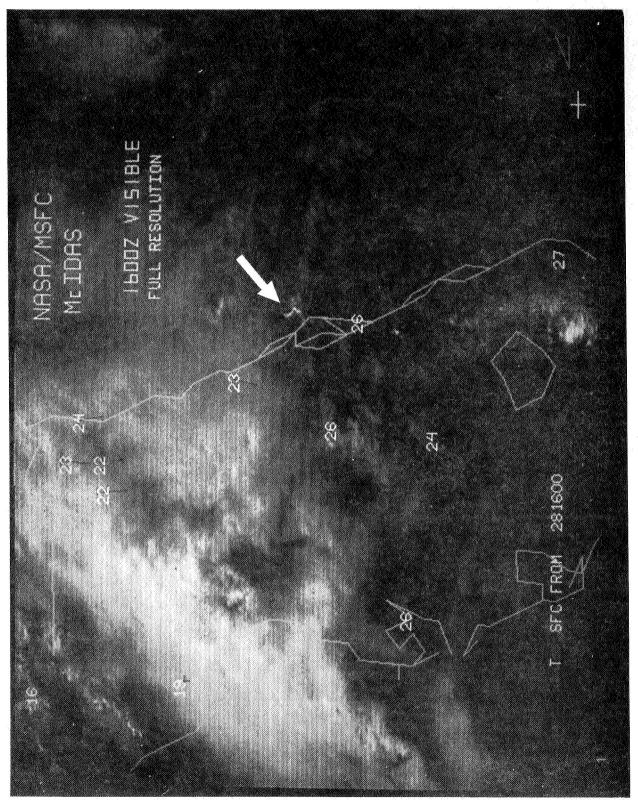


Figure 4. Enlarged view of GOES-5 visible imagery of cloud cover with exhaust trail visible (indicated by arrow) taken at time of launch of STS-9 (1600 UT, November 28, 1983). Surface temperatures and wind barbs for 1600 UT are also included.

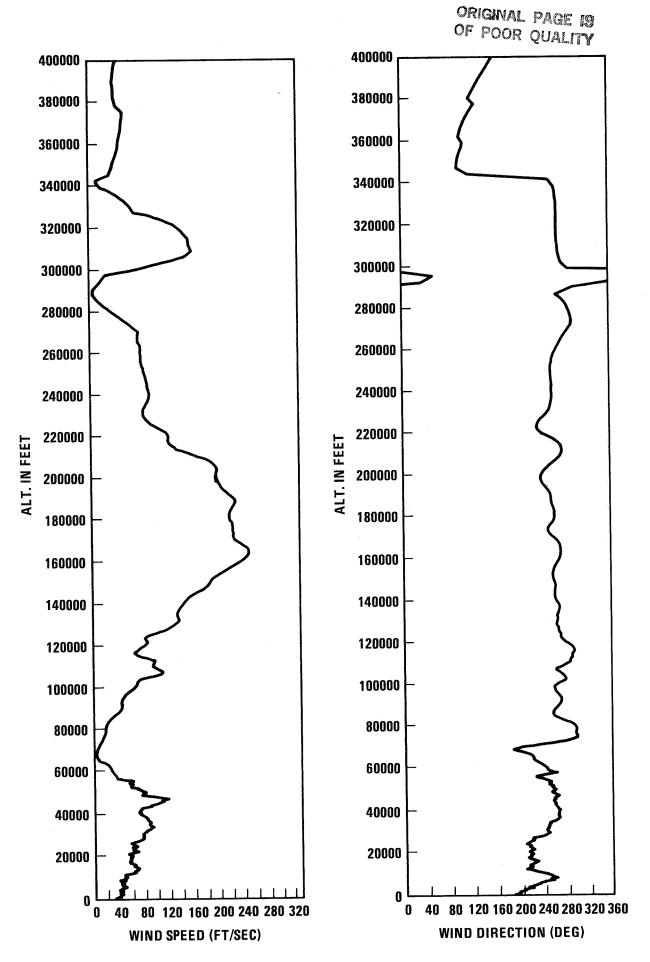


Figure 5. Scalar wind speed and direction at launch time of STS-9.

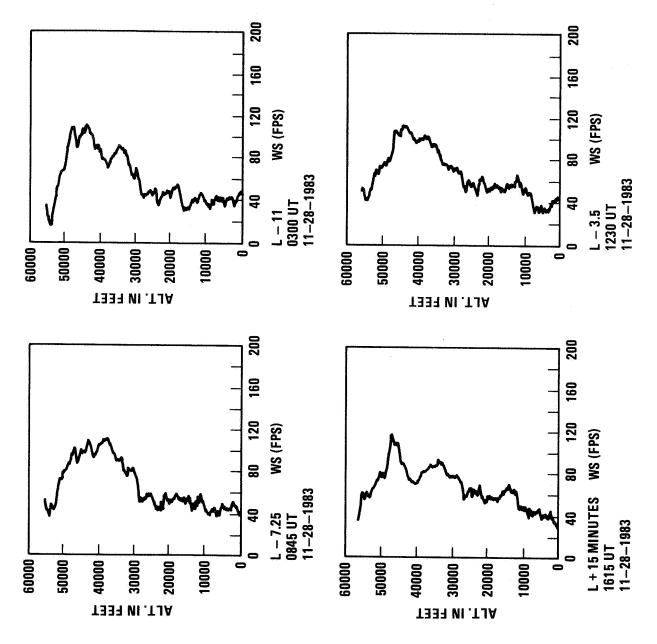


Figure 6. STS-9 prelaunch/launch Jimsphere-measured wind speeds (FPS).

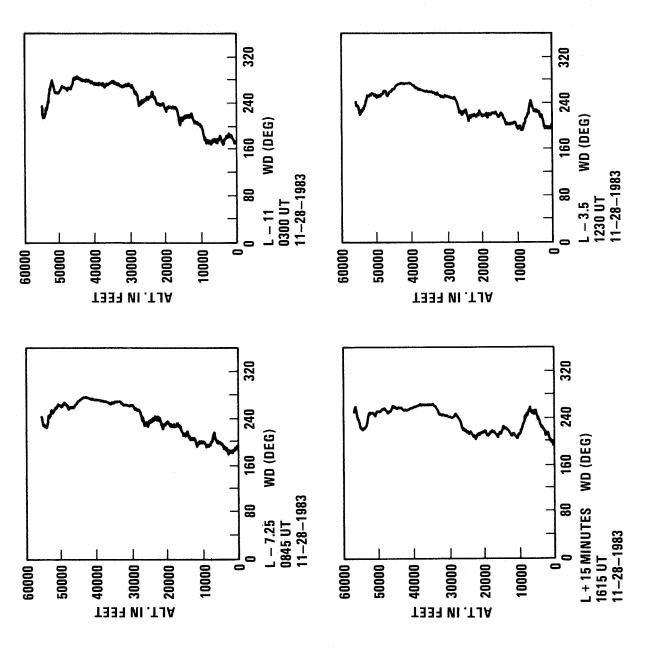
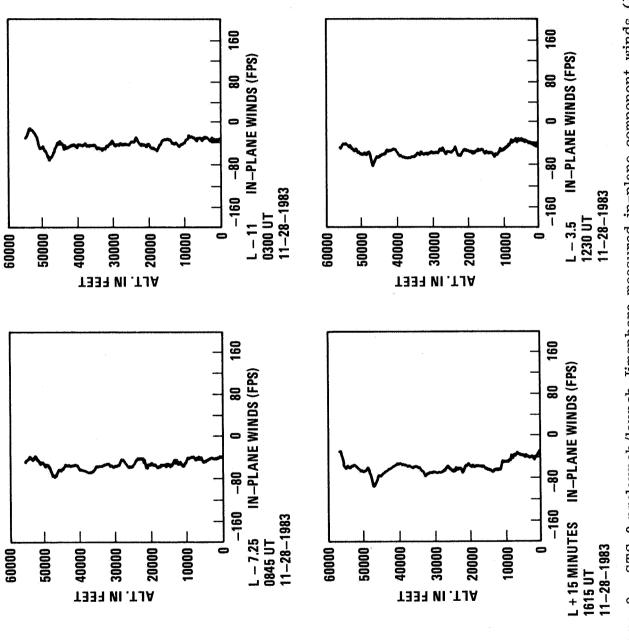
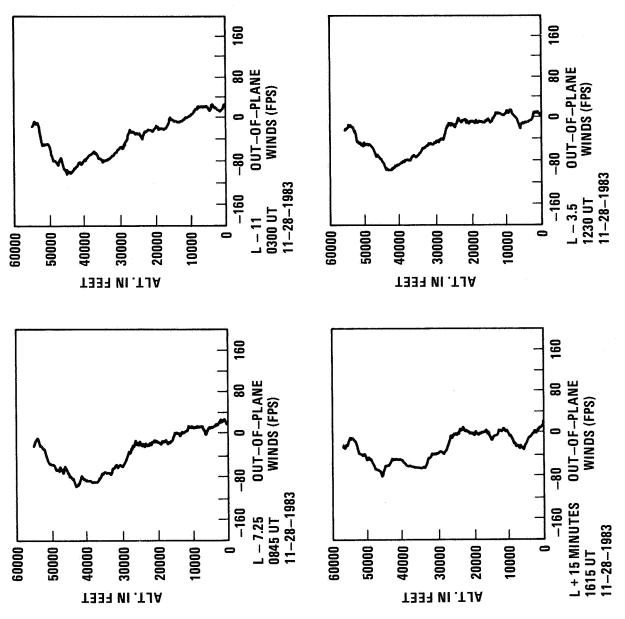


Figure 7. STS-9 prelaunch/launch Jimsphere-measured wind directions (degrees).



STS-9 prelaunch/launch Jimsphere-measured in-plane component winds (FPS). Flight azimuth = 35 degrees. Figure 8.



STS-9 prelaunch/launch Jimsphere-measured out-of-plane component winds (FPS). Flight azimuth = 35 degrees. Figure 9.

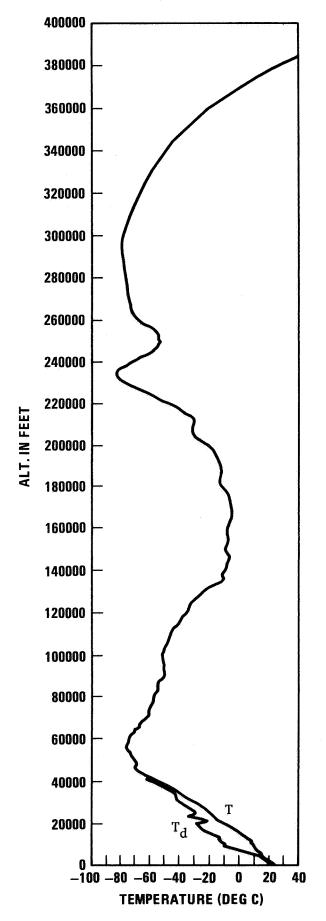


Figure 10. STS-9 temperature profiles versus altitude for launch (ascent).

#### REFERENCES

- 1. Saturn Flight Evaluation Working Group: Saturn Launch Vehicle Flight Evaluation Report Appendix A Atmosphere (A separate report is prepared for each Saturn vehicle launch operation). George C. Marshall Space Flight Center, Alabama.
- 2. Johnson, D. L.: Summary of Atmospheric Data Observations for 155 Flights of MSFC/ABMA Related Aerospace Vehicles. NASA TM X-64796, December 5, 1973.
- 3. Johnson, D. L.: Atmospheric Environment for ASTP (SA-210) Launch. NASA TM X-64990. February 1976.
- 4. Johnson, D. L., Jasper, G., and Brown, S. C.: Atmospheric Environment for Space Shuttle (STS-1) Launch. NASA TM 82436, July 1981.
- 5. Johnson, D. L. and Brown, S. C.: Atmospheric Environment for Space Shuttle (STS-2) Launch. NASA TM 82463, December 1981.
- 6. Johnson, D. L., Brown, S. C., and Batts, G. W.: Atmospheric Environment for Space Shuttle (STS-3) Launch. NASA TM 82480, April 1982.
- 7. Johnson, D. L., Hill, C. K., and Batts, G. W.: Atmospheric Environment for Space Shuttle (STS-4) Launch. NASA TM 82498, July 1982.
- 8. Johnson, D. L., Hill, C. K., and Batts, G. W.: Atmospheric Environment for Space Shuttle (STS-5) Launch. NASA TM 82515, March 1983.
- 9. Johnson, D. L., Hill, C. K., and Batts, G. W.: Atmospheric Environment for Space Shuttle (STS-6) Launch. NASA TM 82529, May 1983.
- 10. Johnson, D. L., Hill, C. K., and Batts, G. W.: Atmospheric Environment for Space Shuttle (STS-7) Launch. NASA TM 82542, July 1983.
- 11. Johnson, D. L., Hill, C. K., Turner, R. E., and Batts, G. W.: Atmospheric Environment for Space Shuttle (STS-8) Launch. NASA TM 82560, October 1983.
- 12. Justus, C. G., et al.: The NASA/MSFC Global Reference Atmosphere Model Mod 3 (with Spherical Harmonic Wind Model). NASA CR-3256, March 1980.
- 13. Smith, O. E. and Weidner, D. K.: A Reference Atmosphere for Patrick AFB, Florida, Annual (1963) Revision). NASA TM X-53139, September 23, 1964.

### APPROVAL

### ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-9) LAUNCH

By D. L. Johnson, C. K. Hill, and G. W. Batts

The information in this report has been reviewed for technical content. Review of any information concerning Department of Defense or nuclear energy activities or programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

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